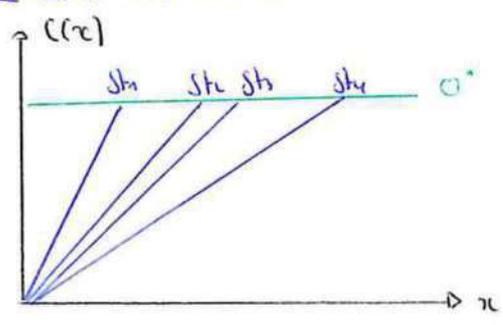


Electrochimie

Semiempirical treatment of the transient response

Potential step under diffusion control

We have to take into account that the thickness of the diffusion layer is a time-dependent quantity: $\delta(t)$ for instance in an unstirred solution.



semiempirical treatment

- Hypotheses and approximations:
- the concentration gradients are still linear in $\delta(t)$
 - Nernstian E process (fast kinetics)

$$\Rightarrow i = -nFA \frac{D_0}{\delta(t)} [O^* - O(c_0)]$$

Experimental conditions: a potential step of magnitude E is applied to an electrode.

At any time, the volume of the diffusion layer is $A\delta(t)$. The number of moles (O_x for instance) in the diffusion layer is given by:

$$\int_0^{\delta} A dx \cdot C(x) = A \int_0^{\delta} C(x) dx$$

volume (x) concentration x

If concentration gradients are linear:

$$\Rightarrow \left(\frac{dO(x)}{dx}\right) = \text{const} = a = \frac{O^* - O(c_0)}{\delta} \text{ and } O(x) = O(c_0) + x \left(\frac{O^* - O(c_0)}{\delta}\right)$$

$$A \int_0^{\delta} O(x) dx = A \int_0^{\delta} \left(O(c_0) + x \left(\frac{O^* - O(c_0)}{\delta}\right)\right) dx = A \left(O(c_0)\delta + (O^* - O(c_0)) \frac{\delta}{2}\right) = \frac{A\delta}{2} (O^* + O(c_0))$$

The number of moles (O_x for instance) in the diffusion layer at a given time is thus given by: $O(t)_s = \frac{A\delta(t)}{2} (O^* + O(c_0))$

The number of moles (O_x for instance) electrolyzed is then given by:

$$A\delta(t)O^* - \frac{A\delta(t)}{2} (O^* + O(c_0)) = \frac{A\delta(t)}{2} (O^* - O(c_0)) = - \int_0^t \frac{i dt}{nF} \text{ since } n_e = \frac{Q}{nF} = \int_0^t \frac{i dt}{nF}$$

i: reduction current

by differentiation: $-\frac{A}{2} (O^* - O(c_0)) \frac{d\delta(t)}{dt} = \frac{i}{nF}$

and we know that: $\frac{i}{nFA} = -D_0 \left(\frac{dO(x)}{dx}\right)_{x=0} = -D_0 \left(\frac{O^* - O(c_0)}{\delta(t)}\right)$ 1st Fick eq

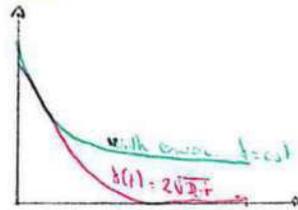
$$\Rightarrow -\frac{A}{2} (O^* - O(c_0)) \frac{d\delta(t)}{dt} = -D_0 \left(\frac{O^* - O(c_0)}{\delta(t)}\right)$$

$$\Rightarrow \frac{A}{2} \frac{d\delta(t)}{dt} = \frac{D_0}{\delta(t)} \text{ or } \frac{A}{2} \delta(t) d\delta(t) = D_0 dt$$

which can be integrated in $\frac{A}{4} \delta^2(t) = D_0 t$ or $\delta^2(t) = 4D_0 t$

knowing how the diffusion layer varies with time, the current then becomes

$$\frac{i}{nFA} = -D_0 \left(\frac{O^* - O(c_0)}{\delta(t)} \right) = -D_0 \left(\frac{O^* - O(c_0)}{\sqrt{2D_0t}} \right) = \frac{-D_0^{1/2}}{\sqrt{2t^{1/2}}} (O^* - O(c_0))$$



This approximate treatment in transient regime predicts:

- The diffusion layer grows with $t^{1/2}$
- The current decays with $t^{-1/2}$

It differs only by a factor of $\sqrt{2/\pi}$ from the rigorous description of current calculated for a Nernstian system during a potential step.

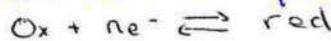
COTTREL EQUATION: $i(t) = \frac{-nFA D_0^{1/2} O^*}{\pi^{1/2} t^{1/2}}$

Rigorous treatment of transient electrochemical responses

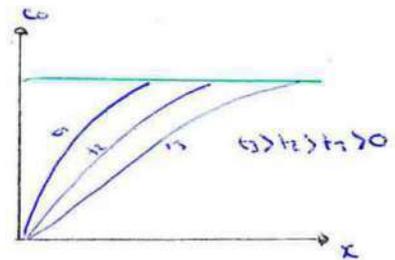
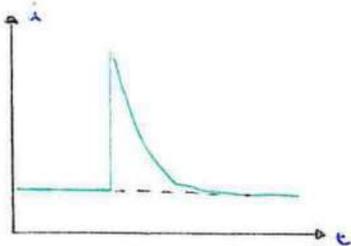
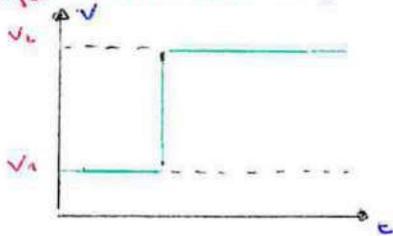
Potential step under diffusion control

Description of the step experiment:

Planar electrode (unidirectional semi-infinite diffusion regime), no stirring instantaneous change in potential from a value where no electrolysis occurs to a value in the non transfer-controlled region:



transfer-controlled region:



- ▶ The concentration is readily = 0 at the electrode surface
- ▶ Current gets under diffusion control
- ▶ Current is independent of E
- ▶ Applies to fast and slow kinetics (activation will of course require a suitable overpotential to reach the non transfer controlled domain).

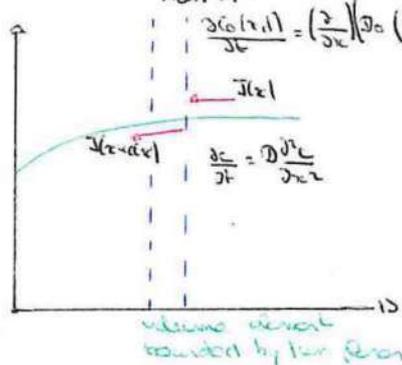
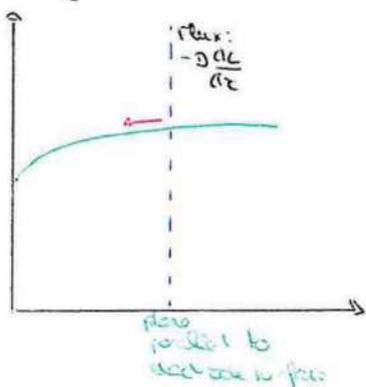
Introduction to the second Fick equation

Linear diffusion to a flat, planar electrode

$$D = \frac{cm^2}{s} \quad (1 \cdot 10^{-5} cm^2 \cdot s^{-1})$$

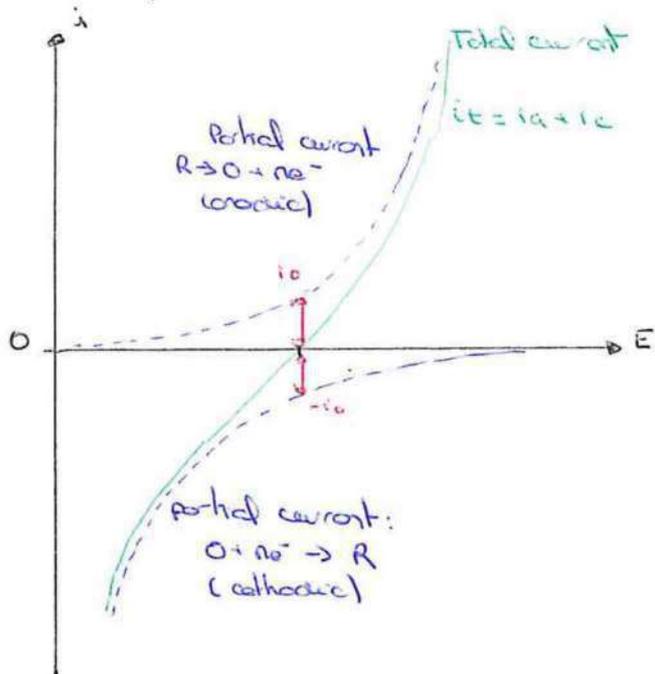
$$Rate = Flux_x = -D \left(\frac{\partial c}{\partial x} \right)_{x=0}$$

$$\frac{\partial c(x,t)}{\partial t} = \left(\frac{\partial}{\partial x} \right) \left(D_0 \left(\frac{\partial c(x,t)}{\partial x} \right) \right)$$



From 1st to 2d Fick equations
 Decrease in concentration over dx.
 $dc(x) = \left(\frac{j(x) - j(x+dx)}{A dx} \right) A dt$
 with: $dt = j(x+dx) - j(x)$
 $\rightarrow \frac{dc(x,t)}{dt} = \frac{-dj}{dx} \Rightarrow \frac{\partial c(x,t)}{\partial t} = D \left(\frac{\partial^2 c(x,t)}{\partial x^2} \right)$

At: $E = E_{eq}$
 $(i_a)_{eq} = (i_c)_{eq} = i_0$



Approximate form of the BV relation

$$i_t = i_0 \left(\exp\left(\frac{\alpha_a n F \eta}{RT}\right) - \exp\left(-\frac{\alpha_r n F \eta}{RT}\right) \right)$$

Even though the net current is zero at equilibrium, the exchange current provides information on the balanced Faradic activity.

i_0 and k^0 characterise the electron transfer kinetic of a given redox couple.

- Fast electron transfer: large values of i_0 and k^0
- Slow electron transfer: small values of i_0 and k^0

The heterogeneous e-transport is considered as being fast when $k^0 > 0.1 \text{ cm}^2 \cdot \text{s}^{-1}$ and slow when $k^0 < 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$

TAFEL equations: Limit cases

When η is highly positive ($\eta \rightarrow +\infty$): oxidation $E > E^{th}$

$$i = i_c = i_0 \left(\exp(\alpha_a n f \eta) - \exp(-\alpha_r n f \eta) \right)$$

$$i \approx i_{ca} = i_0 \exp(\alpha_a n f \eta)$$

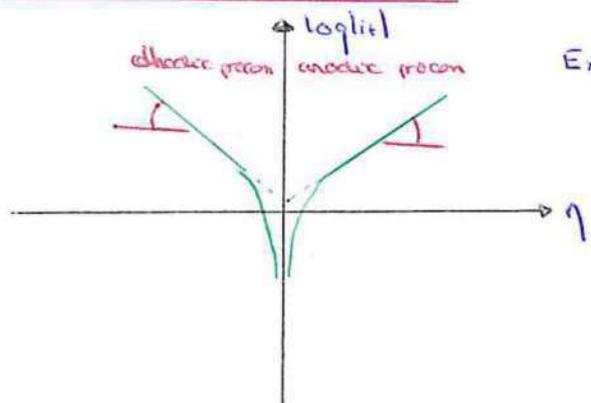
$$\log(i_{ca}) = \log(i_0) + \frac{\alpha_a n f \eta}{2.303} \quad \text{TAFEL EQUATION (anodic)}$$

When η is highly negative ($\eta \rightarrow -\infty$): reduction $E < E^{th}$

$$i = i_c = i_0 \left(\exp(\alpha_a n f \eta) - \exp(-\alpha_r n f \eta) \right)$$

$$i \approx i_{cr} = -i_0 \exp(-\alpha_r n f \eta)$$

$$\log(|i_{cr}|) = \log(i_0) - \frac{\alpha_r n f \eta}{2.303} \quad \text{TAFEL EQUATION (cathodic)}$$



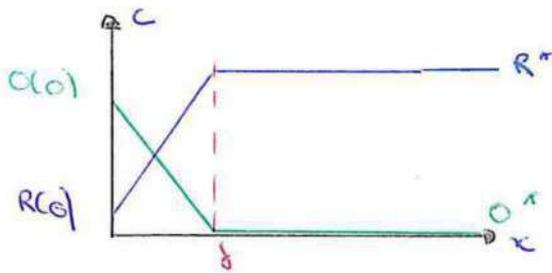
Experimental determination of kinetic parameters: i_0, α_a et α_r

Semi-empirical treatment of steady-state mass transfer for a Nernstian E process

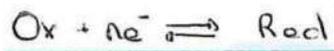
Mass transfer by diffusion is the only limiting process, the flow is determined by the 1st Fick equation:

$$\bar{J}_0(x,t) = -D_0 \frac{\partial O(x,t)}{\partial x}$$

The steady state regime implies that:

$$\left(\frac{\partial C}{\partial t} \right)_x = 0$$


convection is large enough to ensure a continuous replacement at the electrode interface



$$i = nFAJ_0(0) = -nFAD_0 \left(\frac{\partial O(x)}{\partial x} \right)_{x=0} = -nFAm_0 (O^* - O(0))$$

$$i = -nFAJ_R(0) = nFAD_R \left(\frac{\partial R(x)}{\partial x} \right)_{x=0} = nFAm_R (R^* - R(0))$$

For RDE: $m_0 = 0.62 D_0^{2/3} \omega^{1/2} \nu^{-1/6}$

At a disk microelectrode: $m_0 = 4D_0 / (\pi r_0)$

$$\left. \begin{aligned} i_{d,c} &= -nFAm_0 O^* \\ i_{d,a} &= nFAm_R R^* \end{aligned} \right\} \Rightarrow E = E_{O/R}^{0'} + \frac{RT}{nF} \ln \left(\frac{O(0)}{R(0)} \right) = E_{O/R}^{0'} + \frac{RT}{nF} \ln \left(\frac{m_R}{m_0} \right) + \frac{RT}{nF} \ln \left(\frac{i - i_{dc}}{i_{da} - i} \right)$$

Half-wave potential: $E_{1/2} = E \quad i = i_{dc} + i_{da}$

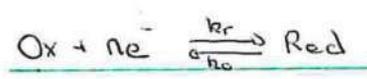
$$\Rightarrow E_{1/2} = E_{O/R}^{0'} + \frac{RT}{nF} \ln \left(\frac{m_R}{m_0} \right)$$

The Levich equation: $i_{d,c} = 0.620 nFA D_0^{2/3} \omega^{1/2} \nu^{-1/6} O^*$

Units: cm² s⁻¹, cm² s⁻¹, rad s⁻¹, mol cm⁻³

Kinetics of the electrochemical reaction: The Butler-Volmer model

k_0 et k_r : kinetic constants associated to the heterogeneous electron transfer (cm s⁻¹).

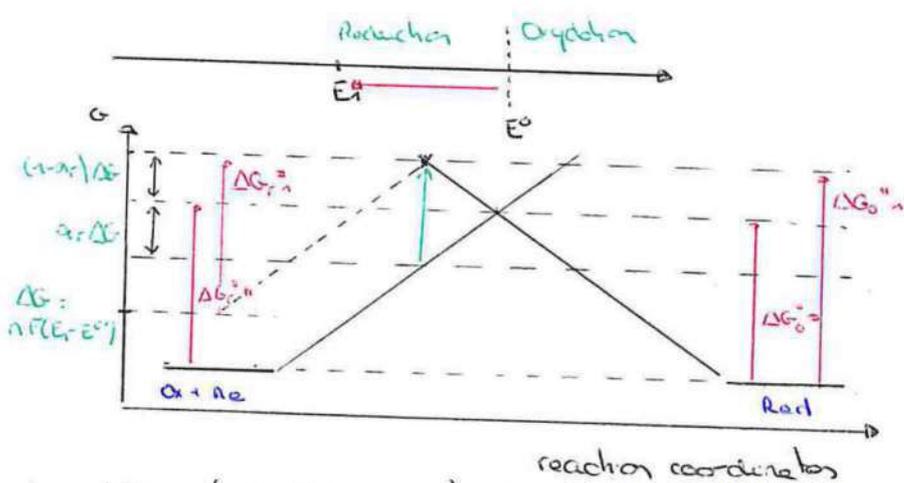


$$(v_{O \rightarrow R})_s = (v_r)_s - (v_o)_s = \frac{-i}{nFA} = k_r O(0) - k_o R(0)$$

$$(v_{R \rightarrow O})_s = (v_o)_s - (v_r)_s = \frac{i}{nFA} = k_o R(0) - k_r O(0)$$

k_0 and k_r depend on the reaction activation barrier and T.

Arrhenius law $k = A \exp \left(-\frac{\Delta G^\ddagger}{RT} \right)$



$$\Delta G_r^\ddagger = \Delta G_r^\circ + \alpha_r nF(E_1 - E^\circ)$$

$$\Delta G_o^\ddagger = \Delta G_o^\circ - nF(1 - \alpha_r)(E_1 - E^\circ)$$

$\alpha_o = 1 - \alpha_r$
 $\alpha_r + \alpha_o = 1$ transport coeff.

$$k_r = k^\circ \exp\left(\frac{-\alpha_r nF}{RT}(E_1 - E^\circ)\right)$$

k° is called the standard rate constant

$$k_o = k^\circ \exp\left(\frac{\alpha_o nF}{RT}(E_1 - E^\circ)\right)$$

Let's consider the special case in which the interface is at equilibrium with a solution in which $O^* = R^*$. In those conditions $E_1 = E^\circ$ and $k_r = k_o = k^\circ$ the net current is zero. E° is thus the potential where the forward and reverse rate constants have the same value.

k° is called the standard rate constant

→ system with a large k° will achieve equilibrium on a short time scale
 → system with a low k° will achieve equilibrium on long time scales.

but: k_r and k_o can still be very large even when k° is low.

$$j = v_o - v_r = \frac{i}{nFA} = k_o R(o) - k_r O(o)$$

$$= \underbrace{R(o)k^\circ \exp\left(\frac{\alpha_o nF(E - E^\circ)}{RT}\right)}_{i_o > 0 \text{ Oxidation}} - \underbrace{O(o)k^\circ \exp\left(\frac{-\alpha_r nF(E - E^\circ)}{RT}\right)}_{i_r < 0 \text{ Reduction}}$$

When $i = 0$, the reduction and oxidation processes proceed at the same speed

$$(i_a)_{eq} = (i_c)_{eq} = i_o \quad E = E_{eq}; R(o) = R^* \text{ and } O(o) = O^*$$

$$i = 0 = nFA k^\circ \left(R^* \exp\left(\frac{\alpha_o nF(E_{eq} - E^\circ)}{RT}\right) - O^* \exp\left(\frac{-\alpha_r nF(E_{eq} - E^\circ)}{RT}\right) \right)$$

$$\frac{i_o}{nFA} = O^* k^\circ \exp\left(\frac{-\alpha_r nF(E_{eq} - E^\circ)}{RT}\right) = R^* k^\circ \exp\left(\frac{\alpha_o nF(E_{eq} - E^\circ)}{RT}\right)$$

$$\frac{i}{nFA} = R(o)k^\circ \exp\left(\frac{\alpha_o nF(E - E_{eq}) + \alpha_o nF(E_{eq} - E^\circ)}{RT}\right) - O(o)k^\circ \exp\left(\frac{-\alpha_r nF(E - E_{eq}) - \alpha_r nF(E_{eq} - E^\circ)}{RT}\right)$$

$$= R(o)k^\circ \exp\left(\frac{\alpha_o nF(E_{eq} - E^\circ)}{RT}\right) \exp\left(\frac{\alpha_o nF\eta}{RT}\right) - O(o)k^\circ \exp\left(\frac{-\alpha_r nF(E_{eq} - E^\circ)}{RT}\right) \exp\left(\frac{-\alpha_r nF\eta}{RT}\right)$$

$$i = \frac{R(o)}{R^*} i_o \exp\left(\frac{\alpha_o nF\eta}{RT}\right) - \frac{O(o)}{O^*} i_o \exp\left(\frac{-\alpha_r nF\eta}{RT}\right)$$

$$= i_o \left(\frac{R(o)}{R^*} \exp\left(\frac{\alpha_o nF\eta}{RT}\right) - \frac{O(o)}{O^*} \exp\left(\frac{-\alpha_r nF\eta}{RT}\right) \right)$$

The electron transfer controls the kinetics
 → CT current.

if $O(o) = O^*$ and $R(o) = R^*$ (upon neglecting the mass-transfer effects). If the solution is well stirred, or currents are kept so low that the surface concentrations do not differ appreciably from the bulk values. Reasonable approximations... i is lower than about 10% of limit diff.

The $C(x,t)$ function can be used to solve the first Fick equation. $\bar{J}_0(0,t) = -D_0 \left(\frac{\partial C_0(x,t)}{\partial x} \right)_{x=0}$
 Using $C_0(x,t) = C_0^* \operatorname{erfc} \left(\frac{x}{2\sqrt{Dt}} \right)$ and $i(t) = nFA\bar{J}_0(0,t) = -nFAD_0 \left(\frac{\partial C_0(x,t)}{\partial x} \right)_{x=0} > 0$

The derivation can be made easily using the transformed functions.

$$\bar{C}_0(x,s) = \frac{C_0^*}{s} - \frac{C_0^*}{s} \exp \left(-\sqrt{\frac{s}{D}} x \right) \quad \text{and} \quad \bar{i}(s) = nFA\bar{J}_0(0,s) = -nFAD_0 \left(\frac{\partial \bar{C}_0(x,s)}{\partial x} \right)_{x=0}$$

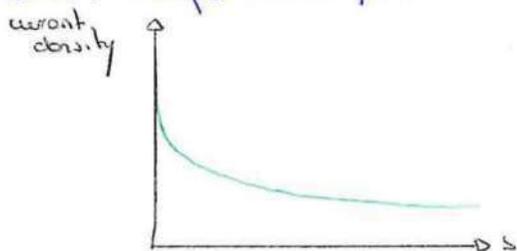
$$\bar{i}(s) = -nFAD_0 \left(\frac{\partial \bar{C}_0(x,s)}{\partial x} \right)_{x=0} = -\frac{nFAD_0 C_0^*}{s} \sqrt{\frac{s}{D}} \exp \left(-\sqrt{\frac{s}{D}} x \right)_{x=0} = \frac{-nFAD_0^{1/2} C_0^*}{s^{1/2}}$$

$$\stackrel{\mathcal{L}^{-1}}{\Rightarrow} i(t) = \frac{-nFAD_0^{1/2} C_0^*}{\pi^{1/2} t^{1/2}} \quad \text{COTTREL EQUATION}$$

The $1/t^{1/2}$ dependence is a mark of diffusive control over the rate of electrodeysis.

Limitation in Cottrel experiments

- Ohmic drop/compensate affects (R_u, C_d): Non faradic current may also flow during potential step experiments. This current decays exponentially with a cell time constant, $R_u C_d$ where R_u is the uncompensated resistance and C_d is the double-layer capacitance. This contribution might interfere



For reduction

$$[i(t)]_r = \frac{-nFAD_0^{1/2} C_0^*}{\pi^{1/2} t^{1/2}}$$

For oxidation

$$[i(t)]_o = \frac{nFAD_0^{1/2} C_{R^*}}{\pi^{1/2} t^{1/2}}$$

\Rightarrow Determination of diffusion coefficients

Case of a spherical electrode

Experimental conditions: a potential step of magnitude E is applied to a spherical electrode. This potential is large enough to ensure $C(r,0) = 0$ for $t > 0$.

The Fick equation in spherical coordinates becomes: $\frac{\partial C(r,t)}{\partial t} = D \left(\frac{\partial^2 C(r,t)}{\partial r^2} + \frac{2}{r} \frac{\partial C(r,t)}{\partial r} \right)$

Changing the variable from $C(r,t)$ to $u(r,t)$ using $u(r,t) = rC(r,t)$ with $r = \text{const}$ allows to simplify the eq:

$$(r^{-1}u)'' = r^{-1}u'' + 2u'(r^{-1})' + u(r^{-1})'' = r^{-1}u'' - 2r^{-2}u' + 2r^{-3}u$$

$$(ur^{-1})' = \left(\frac{u}{r} \right)' = \frac{ur' - ur''}{r^2} = \frac{u'r - u}{r^2} = u'r^{-1} - ur^{-2}$$

$$\Rightarrow D(r^{-1}u'' - 2r^{-2}u' + 2r^{-3}u + 2r^{-1}(u'r^{-1} - ur^{-2})) = D(r^{-1}u'' - 2r^{-2}u' + 2r^{-3}u + 2r^{-2}u' - 2r^{-3}u) = D(r^{-1}u'')$$

$$\begin{aligned} \frac{\partial C(r,t)}{\partial t} &= \frac{1}{r} \frac{\partial u(r,t)}{\partial t} \\ \frac{\partial^2 C(r,t)}{\partial r^2} &= \frac{\partial^2}{\partial r^2} \left(\frac{u(r,t)}{r} \right) = (r^{-1}u)'' \\ \frac{2}{r} \frac{\partial C(r,t)}{\partial r} &= \frac{2}{r} \frac{\partial}{\partial r} \left(\frac{u(r,t)}{r} \right) = 2r^{-1}(r^{-1}u)' \\ \left(\frac{u}{r} \right)' &= \frac{1}{r} u' - \frac{u}{r^2} \quad (u/r)'' = \frac{1}{r} u'' - 2 \frac{u'}{r^2} + \frac{2u}{r^3} \end{aligned}$$

$$\frac{\partial C(r,t)}{\partial t} = D \left(\frac{\partial^2 C(r,t)}{\partial r^2} + \frac{2}{r} \frac{\partial C(r,t)}{\partial r} \right) \Rightarrow \frac{\partial u(r,t)}{\partial t} = D \left(\frac{\partial^2 u(r,t)}{\partial r^2} \right)$$

$$\mathcal{L} \left\{ \frac{\partial u(r,t)}{\partial t} \right\} = \mathcal{L} \left\{ D \frac{\partial^2 u(r,t)}{\partial r^2} \right\}$$

$$\int_0^\infty e^{-st} \frac{\partial u(r,t)}{\partial t} dt = D \int_0^\infty e^{-st} \frac{\partial^2 u(r,t)}{\partial r^2} dt = D \frac{\partial^2}{\partial r^2} \int_0^\infty e^{-st} u(r,t) dt = D \frac{d^2 \bar{u}(r,s)}{dr^2}$$

$$s\bar{u}(r,s) - u(r,0) = D \frac{d^2 \bar{u}(r,s)}{dr^2} \quad \text{and with the boundary condition } C(r,0) = 0 \Rightarrow u(r,0) = rC = 0$$

$$s\bar{u}(r,s) - rC^* = D \frac{d^2 \bar{u}(r,s)}{dr^2} \Rightarrow \frac{d^2 \bar{u}(r,s)}{dr^2} - \frac{s}{D} \bar{u}(r,s) + \frac{rC^*}{D} = 0 \Rightarrow \bar{u}(r,s) = \frac{rC^*}{s} + A \exp \left(-\sqrt{\frac{s}{D}} r \right) + B \exp \left(\sqrt{\frac{s}{D}} r \right)$$

Experimental conditions: a potential step of magnitude E is applied to an electrode. calculation of the diffusion-limited current and of the concentration profile, $C(x,t)$ involves the solution of the linear diffusion equation (unidirectional diffusion regime)

$$\frac{\partial C(x,t)}{\partial t} = D \frac{\partial^2 C(x,t)}{\partial x^2} \quad \text{eq 1}$$

Boundary conditions are needed (only 0₂ present)
 $C(x,0) = C^*$ $\lim_{x \rightarrow \infty} C(x,t) = C^*$ $C(0,t) = 0 \text{ for } t > 0$

Transforming eq 1 using Laplace Transformation leads to: $L\left(\frac{\partial C(x,t)}{\partial t}\right) = L\left(D \frac{\partial^2 C(x,t)}{\partial x^2}\right)$

$$\int_0^\infty e^{-st} \frac{\partial C(x,t)}{\partial t} dt = D \int_0^\infty e^{-st} \frac{\partial^2 C(x,t)}{\partial x^2} dt = D \frac{\partial^2}{\partial x^2} \int_0^\infty e^{-st} C(x,t) dt = D \frac{d^2 \bar{C}(x,s)}{dx^2}$$

$$L\left(\frac{\partial C(x,t)}{\partial t}\right) = s\bar{C}(x,s) - C(x,0) = D \frac{d^2 \bar{C}(x,s)}{dx^2} \quad \text{and with the boundary condition } C(x,0) = C^*$$

$$\Rightarrow s\bar{C}(x,s) - C^* = D \frac{d^2 \bar{C}(x,s)}{dx^2}$$

$$\Rightarrow \frac{d^2 \bar{C}(x,s)}{dx^2} - \frac{s}{D} \bar{C}(x,s) = -\frac{C^*}{D} \quad \text{How to solve such equation? LT makes it possible.}$$

let's set: $\bar{C}(x,s) = u(x)$ which can be submitted to a second transformation

$$L\left\{\frac{d^2 u(x)}{dx^2}\right\} = s'^2 \bar{u}(s') - s' u(0) - u'(0)$$

$$L\left\{\frac{s}{D} u(x)\right\} = \frac{s}{D} \bar{u}(s') \quad L\{1\} = \frac{1}{s'}$$

$$\frac{d^2 u(x)}{dx^2} - \frac{s}{D} u(x) + \frac{C^*}{D} = 0$$

$$s'^2 \bar{u}(s') - s' u(0) - u'(0) - \frac{s}{D} \bar{u}(s') + \frac{C^*}{D s'} = 0$$

$$\bar{u}(s') \left(s'^2 - \frac{s}{D}\right) = s' u(0) + u'(0) - \frac{C^*}{D s'}$$

$$\bar{u}(s') \left(s'^2 - \frac{s s'}{D}\right) = s'^2 u(0) + u'(0) s' - \frac{C^*}{D}$$

$$\bar{u}(s') = \frac{s'^2 u(0) + s' u'(0) - \frac{C^*}{D}}{s' \left(s'^2 - \frac{s}{D}\right)} = \frac{s'^2 u(0) + s' u'(0) - \frac{C^*}{D}}{s' \left(s' - \sqrt{\frac{s}{D}}\right) \left(s' + \sqrt{\frac{s}{D}}\right)}$$

$$\bar{u}(s') = \frac{B'}{s' - \sqrt{\frac{s}{D}}} + \frac{A'}{s' + \sqrt{\frac{s}{D}}} + \frac{E'}{s'}$$

$$\bar{u}(s') = \frac{s'^2 (B' + A' + E') + s' \sqrt{\frac{s}{D}} (B' - A') + \frac{E' s}{D}}{(s' - \sqrt{\frac{s}{D}}) (s' + \sqrt{\frac{s}{D}}) s'} \Rightarrow \frac{E' s}{D} = \frac{C^*}{D} \Rightarrow E' = \frac{C^*}{s}$$

$$L^{-1} \rightarrow L^{-1}\{\bar{u}(s')\} = L^{-1}\left\{\frac{B'}{s' - \sqrt{\frac{s}{D}}}\right\} + L^{-1}\left\{\frac{A'}{s' + \sqrt{\frac{s}{D}}}\right\} + L^{-1}\left\{\frac{E'}{s'}\right\}$$

$$u(x) = \bar{C}(x,s) = E' + A' \exp\left(-\sqrt{\frac{s}{D}} x\right) + B' \exp\left(\sqrt{\frac{s}{D}} x\right) \quad \text{with } E' = \frac{C^*}{s}$$

$$\frac{d^2 \bar{C}(x,s)}{dx^2} - \frac{s}{D} \bar{C}(x,s) + \frac{C^*}{D} = 0 \quad \Rightarrow \quad \bar{C}(x,s) = \frac{C^*}{s} + A' \exp\left(-\sqrt{\frac{s}{D}} x\right) + B' \exp\left(\sqrt{\frac{s}{D}} x\right)$$

$C(x,t)$ tends towards a finite value when $x \rightarrow \infty$ and so does $\bar{C}(x,s) \Rightarrow B' = 0$

Determination of A' using known boundary conditions

$$C(x,0) = C^* \quad C(0,t) = 0 \text{ for } t > 0$$

$$\lim_{x \rightarrow \infty} C(x,t) = C^*$$

$$\bar{C}(x,s) = \frac{C^*}{s} + A' \exp\left(-\sqrt{\frac{s}{D}} x\right)$$

$$\bar{C}(0,s) = 0 \text{ leads to } \frac{C^*}{s} + A' = 0 \text{ and } A' = -\frac{C^*}{s} \Rightarrow \bar{C}(x,s) = \frac{C^*}{s} - \frac{C^*}{s} \exp\left(-\sqrt{\frac{s}{D}} x\right)$$

from the table of Laplace transformation we know that $L^{-1}\left\{L^{-1}\left\{s'^2 \exp\left(-\sqrt{\frac{s}{D}} x\right)\right\}\right\} = \text{erfc}\left(\frac{x}{\sqrt{4Dt}}\right)$

$$\bar{C}(x,s) = \frac{C^*}{s} - \frac{C^*}{s} \exp\left(-\sqrt{\frac{s}{D}} x\right) \Rightarrow C(x,t) = C^* - C^* \text{erfc}\left(\frac{x}{\sqrt{4Dt}}\right) = C^* \text{erfc}\left(\frac{x}{\sqrt{4Dt}}\right)$$

Sigmoid shaped function occurring in probability, statistics, and partial differential equations describing diffusion.

Error function: $\text{erf}(x) = \frac{2}{\sqrt{\pi}} \int_0^x \exp(-t^2) dt$

complementary error function: $\text{erfc}(x) = 1 - \text{erf}(x)$

$C(r,t)$ tends towards a finite value when $x \rightarrow \infty$ and so does $\bar{u}(r,s) \Rightarrow B' = 0$

Determination of A' using known boundary conditions

$$\bar{u}(r,s) = \frac{rC^*}{s} + A' \exp\left(-\sqrt{\frac{s}{D}} r\right)$$

$$C(r^0, t) = 0 \text{ for } t > 0 \Rightarrow \bar{u}(r^0, s) = 0$$

$\bar{u}(r^0, s) = 0$ leads to $\frac{r^0 C^*}{s} + A' \exp\left(-\sqrt{\frac{s}{D}} r^0\right) = 0$ and $A' = -\frac{r^0 C^*}{s} \exp\left(\sqrt{\frac{s}{D}} r^0\right)$

$$\Rightarrow \bar{u}(r,s) = r \bar{C}(r,s) = \frac{rC^*}{s} - \frac{r^0 C^*}{s} \exp\left(-\sqrt{\frac{s}{D}} (r-r^0)\right) \Rightarrow \bar{C}(r,s) = \frac{C^*}{s} - \frac{r^0 C^*}{rs} \exp\left(-\sqrt{\frac{s}{D}} (r-r^0)\right)$$

The $C(r,t)$ function can be used to solve the first Fick equation

$$J_0(r^0, t) = -D_0 \left(\frac{\partial C_0(r,t)}{\partial r} \right)_{r=r^0}$$

using $i(t) = nFAJ_0(r^0, t) = -nFAD_0 \left(\frac{\partial C_0(r,t)}{\partial r} \right)_{r=r^0}$

This derivation can be made easily using the transformed function.

$$\bar{C}(r,s) = \frac{C^*}{s} - \frac{r^0 C^*}{rs} \exp\left(-\sqrt{\frac{s}{D}} (r-r^0)\right) \text{ and } \bar{i}(s) = nFAJ_0(r^0, s) = -nFAD_0 \left(\frac{\partial \bar{C}_0(r,s)}{\partial r} \right)_{r=r^0}$$

$$\left(\frac{\partial \bar{C}_0(r,s)}{\partial r} \right)_{r=r^0} = -\frac{r^0 C^*}{s} \left(-\frac{1}{r^2} \exp\left(-\sqrt{\frac{s}{D}} (r-r^0)\right) + \frac{1}{r} \left(-\sqrt{\frac{s}{D}}\right) \exp\left(-\sqrt{\frac{s}{D}} (r-r^0)\right) \right)$$

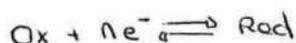
$$= -\frac{r^0 C^*}{s} \left(-\frac{1}{r^2} - \frac{1}{r^0} \sqrt{\frac{s}{D}} \right) = \frac{r^0 C^*}{r^0 s} + \frac{r^0 C^*}{s r^0} \sqrt{\frac{s}{D}} = \frac{C^*}{r^0 s} + \frac{C^*}{\sqrt{sD}}$$

$$\bar{i}(s) = -nFAD_0 C^* \left(\frac{1}{r^0 s} + \frac{1}{\sqrt{sD}} \right) \xrightarrow{\text{TL}^{-1}} i(t) = -nFAD_0 C^* \left(\frac{1}{r^0} + \frac{1}{(D_0 \pi t)^{1/2}} \right)$$

$$i_d(\text{spherical}) = i_d(\text{linear}) = \frac{nFAD_0 C^*}{r^0}$$

$$\lim_{t \rightarrow \infty} i_d(\text{spherical}) = \frac{nFAD_0 C^*}{r^0}$$

Linear sweep voltammetry for a simple Nernstian E process

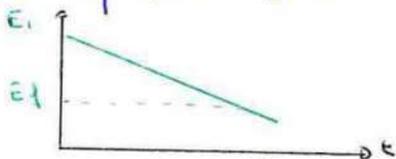


Description of the sweep experiment:

Planar electrode (under a diffusion semi-infinite diffusion regime), no stirring. The potential is initially set to a value where no reaction occurs (open circuit potential). The potential is step linearly at a given scan rate v (V/s).

Case of a reduction: Ox is the only species present in solution $E_i \gg E^0$

$$E = E_i - v \cdot t$$



Boundary conditions: $C_0(r, 0) = C^*$ $\lim_{t \rightarrow \infty} C_0(r, t) = C^*$
 $C_R(r, 0) = 0$ $\lim_{t \rightarrow \infty} C_R(r, t) = 0$
 $D_O \left(\frac{\partial C_O}{\partial r} \right)_{r=0} + D_R \left(\frac{\partial C_R}{\partial r} \right)_{r=0} = 0$

The system is Nernstian (fast ET rate):

The concentration of Ox and Red adjust at the electrode surface according to the Nernst equation.

$$\frac{C_O(0,t)}{C_R(0,t)} = \exp\left(\frac{nF}{RT} (E - E^0)\right) \Rightarrow \frac{C_O(0,t)}{C_R(0,t)} = \exp\left(\frac{nF}{RT} (E_i - vt - E^0)\right)$$

The concentration ratio now depends on time. This is the main difference with constant potential experiments.

Charging notations:

$$\frac{C_O(0,t)}{C_R(0,t)} = \exp\left(\frac{nF}{RT} (E_i - E^0)\right) \exp\left(-\frac{nF}{RT} vt\right) = \Theta_0 \exp(-\gamma t) = \Theta_0 S(t) \text{ with}$$

$$\Theta_0 = \exp\left(\frac{nF}{RT} (E_i - E^0)\right) \text{ Fixed value}$$

$$\gamma = \frac{nF}{RT} v \text{ passively variable value}$$

Solving the Fick equations with TL gives the L {concentrations}

$$\frac{\partial C_O(x,t)}{\partial t} = D_O \frac{\partial^2 C_O(x,t)}{\partial x^2} \quad \xrightarrow{TL} \quad \bar{C}_O(x,s) = \frac{C_O^*}{s} + A_O(s) \exp(-\sqrt{\frac{s}{D_O}} x) \quad \text{since } C_O^* = 0$$

$$\frac{\partial C_R(x,t)}{\partial t} = D_R \frac{\partial^2 C_R(x,t)}{\partial x^2} \quad \xrightarrow{TL} \quad \bar{C}_R(x,s) = \frac{C_R^*}{s} + A_R(s) \exp(-\sqrt{\frac{s}{D_R}} x) = A_R(s) \exp(-\sqrt{\frac{s}{D_R}} x)$$

L {Current} then becomes

$$\bar{i}(s) = nFAj_0(0,s) = -nFAD_O \left(\frac{\partial \bar{C}_O(x,s)}{\partial x} \right)_{x=0} \quad \text{with} \quad \left(\frac{\partial \bar{C}_O(x,s)}{\partial x} \right)_{x=0} = -\sqrt{\frac{s}{D_O}} A_O(s) \exp(-\sqrt{\frac{s}{D_O}} x)$$

$$\Rightarrow \bar{i}(s) = -nFAD_O \left(\frac{\partial \bar{C}_O(x,s)}{\partial x} \right)_{x=0} = nFAD_O \sqrt{\frac{s}{D_O}} A_O(s) = nFA\sqrt{D_O s} A_O(s) \Rightarrow A_O(s) = \frac{\bar{i}(s)}{nFA(D_O s)^{1/2}}$$

$$\Rightarrow \bar{C}_O(x,s) = \frac{C_O^*}{s} + \frac{\bar{i}(s)}{nFA(D_O s)^{1/2}} \exp(-\sqrt{\frac{s}{D_O}} x) \quad \text{and} \quad \bar{C}_O(0,s) = \frac{C_O^*}{s} + \frac{\bar{i}(s)}{nFA(D_O s)^{1/2}}$$

$\bar{C}_O(0,s) = \frac{C_O^*}{s} + \frac{\bar{i}(s)}{nFA(D_O s)^{1/2}}$ Inversion of the transform cannot be carried out from tabulated functions.

One can obtain it from the convolution integral:

Upon setting $g(s) = \bar{i}(s)$ and $h(s) = \frac{1}{s^{1/2}}$

$$\bar{C}_O(0,s) = \frac{C_O^*}{s} + \frac{1}{nFA(D_O s)^{1/2}} (h(s) \times g(s))$$

$L^{-1}\{h(s) \times g(s)\} = h(t) \times g(t)$ The star represents the convolution integral $\int_0^t h(t-\tau) g(\tau) d\tau$ the convolution integral $\tau =$ auxiliary variable.

Then knowing that $L\{i(t)\} = \bar{i}(s)$ and $L\left\{\frac{1}{(\pi t)^{1/2}}\right\} = \frac{1}{s^{1/2}}$

$$\Rightarrow L^{-1}\{\bar{C}_O(0,s)\} = C_O(0,t) = C_O^* + \frac{1}{nFA(\pi D_O)^{1/2}} \int_0^t (t-\tau)^{-1/2} i(\tau) d\tau$$

$$C_O(0,t) = C_O^* - \frac{1}{(\pi D_O)^{1/2}} \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau \quad \text{with} \quad f(\tau) = \frac{-i(\tau)}{nFA}$$

And one can similarly demonstrate that, knowing that:

$$\frac{C_O(0,t)}{C_R(0,t)} = \exp\left(\frac{nF}{RT}(E_t - E^{\circ'})\right) \exp\left(-\frac{nF}{RT} \sigma t\right) = \theta_0 \exp(-\sigma t) = \theta_0 S(t)$$

NB: $\int_0^t (t-\tau)^{-1/2} f(\tau) d\tau$ is also called the convoluted current noted $\bar{i}(t)$
 $\Rightarrow C_O(0,t) = C_O^* - \frac{\bar{i}(t)}{(\pi D_O)^{1/2}}$

(which means that the σt is dimensionless and that E varies linearly with t)

$$\Rightarrow \frac{C_O(0,t)}{C_R(0,t)} = \frac{C_O^* - \frac{\bar{i}(t)}{(\pi D_O)^{1/2}}}{\frac{\bar{i}(t)}{(\pi D_R)^{1/2}}}$$

$$C_O^* - \frac{1}{(\pi D_O)^{1/2}} \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau = \theta_0 S(t) \frac{1}{(\pi D_R)^{1/2}} \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau$$

$$C_O^* = \left(\theta_0 S(t) \frac{1}{(\pi D_R)^{1/2}} + \frac{1}{(\pi D_O)^{1/2}} \right) \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau \Rightarrow \frac{C_O^*}{\theta_0 S(t) \frac{1}{(\pi D_R)^{1/2}} + \frac{1}{(\pi D_O)^{1/2}}} = \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau$$

$$\frac{nFA(\pi D_O)^{1/2} C_O^*}{\theta_0 S(t) \left(\frac{D_O}{D_R}\right)^{1/2} + 1} = - \int_0^t (t-\tau)^{-1/2} i(\tau) d\tau$$

$$\frac{nFA(\pi D_O)^{1/2} C_O^*}{\theta_0 S(t) f + 1} = - \int_0^t (t-\tau)^{-1/2} i(\tau) d\tau \quad \text{No exact solution to this equation, requires a numerical treatment.}$$

Since the goal is to calculate current-potential curves rather than current-time curves it is more convenient to change from $i(t)$ to $i(E)$. To go from $i(t)$ to $i(E)$ we use the following change in variable $\tau \rightarrow \sigma t$ σ is a dimensionless and proportional to potential

$$\sigma t \begin{cases} f(t) = g(\sigma t) \\ \text{and we note } z = \sigma \tau = \frac{nF}{RT} \sigma \tau \Rightarrow dz = \sigma d\tau \end{cases}$$

$$\text{with: } \begin{cases} \sigma t = \frac{nF}{RT} \sigma t \text{ and } E = E_1 - \sigma t \\ f(t) = \frac{-i(t)}{nFA} \end{cases}$$

$$\frac{(\pi D_O)^{1/2} C_O^*}{\theta_0 S(t) f + 1} = \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau$$

$$\int_0^t (t-\tau)^{-1/2} f(\tau) d\tau = \int_0^{\sigma t} (t-\tau)^{-1/2} g(\sigma \tau) d\tau = \int_0^{\sigma t} \left(t - \frac{z}{\sigma}\right)^{-1/2} g(z) \frac{dz}{\sigma}$$

$$\frac{1}{\sigma} \int_0^{\sigma t} \left(\frac{\sigma t - z}{\sigma}\right)^{-1/2} g(z) dz = \frac{1}{\sigma} \left(\frac{1}{\sigma}\right)^{-1/2} \int_0^{\sigma t} (\sigma t - z)^{-1/2} g(z) dz = \left(\frac{1}{\sigma}\right)^{1/2} \int_0^{\sigma t} (\sigma t - z)^{-1/2} g(z) dz$$

$$= \sigma^{-1/2} \int_0^{\sigma t} (\sigma t - z)^{-1/2} g(z) dz$$

$$\frac{(\pi D_O)^{1/2} C_O^*}{\theta_0 S(t) f + 1} = \sigma^{-1/2} \int_0^{\sigma t} (\sigma t - z)^{-1/2} g(z) dz$$

his integral can be made dimensionless using

$$\chi(z) = \frac{g(z)}{(\pi D_0 \sigma)^{1/2} C_0^*}$$

$$\frac{1}{\theta_0 S(\sigma) f + 1} = \int_0^{\sigma} (\sigma - z)^{-1/2} \chi(z) dz = \int_0^{\sigma} \frac{\chi(z)}{(\sigma - z)^{1/2}} dz \Rightarrow \frac{1}{\theta_0 S(\sigma) f + 1} = \int_0^{\sigma} \frac{\chi(z)}{(\sigma - z)^{1/2}} dz$$

And since: $\begin{cases} f(t) = -\frac{i(t)}{nFA} \\ f(z) = g(\sigma z) = g(\beta) \end{cases} \Rightarrow \begin{cases} g(z) = (\pi D_0 \sigma)^{1/2} C_0^* \chi(\beta) \\ g(z) = g(\sigma z) = (\pi D_0 \sigma)^{1/2} C_0^* \chi(\sigma z) \end{cases}$ This integral provides values of $\chi(\sigma t)$ as a function of σt .

$i = -nFA(\pi D_0 \sigma)^{1/2} C_0^* \chi(\sigma t)$ $\frac{1}{\theta_0 S(\sigma) f + 1} = \int_0^{\sigma} \frac{\chi(z)}{(\sigma - z)^{1/2}} dz$

for a given value of E at t, $S(\sigma t)$ can be calculated which leads to $\chi(\sigma t)$ and then to the current $i(t)$

$S(t) = \exp\left(-\frac{nF}{RT} \sigma t\right) = \exp(-\sigma t) \Rightarrow \frac{1}{\theta_0 S(\sigma t) f + 1} = \int_0^{\sigma} \frac{\chi(z)}{(\sigma - z)^{1/2}} dz \Rightarrow i(t) = -nFA(\pi D_0 \sigma)^{1/2} C_0^* \chi(\sigma t)$

$\pi^{1/2} \chi(\sigma t)$ reaches a maximum where $\pi^{1/2} \chi(\sigma t) = 0.4463$ at $E = E_{peak}$

$i_{peak, cathodic} = -0.4463 \times nFA \left(\frac{D_0 n F v}{RT}\right)^{1/2} C_0^* = -0.4463 \times nFA \left(\frac{nF}{RT}\right)^{1/2} D_0^{1/2} v^{1/2} C_0^*$

Randles-Sevcik equation: $i_{p,c} = (2.69 \cdot 10^5) n^{3/2} A D_0^{1/2} v^{1/2} C_0^*$

The potential value E_{peak} corresponding to $i_{p,c}$ can be calculated

$E_{p,c} = E^v - \frac{RT}{nF} \ln f = 1.109 \frac{RT}{nF} \quad f = \left(\frac{D_0}{D_R}\right)^{1/2}$

$E_{p,c} = E_{1/2} - 1.109 \frac{RT}{nF} = E_{1/2} - \frac{0.0255 V}{n}$ at 25°C found from numerical treatments

$\Rightarrow E_{peak}$ is invariant with concentration and scan rate

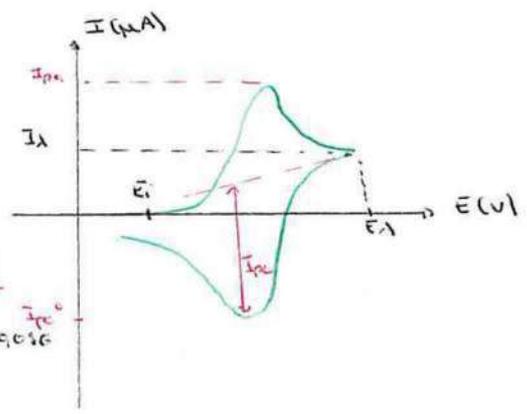
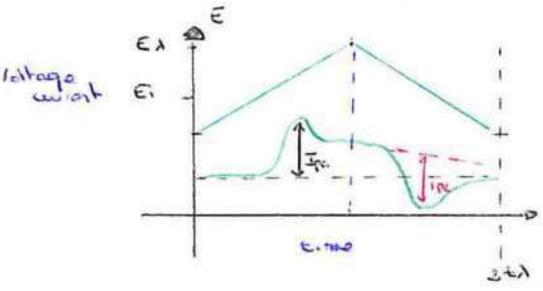
$\Rightarrow i_{peak}$ varies with $v^{1/2}$ which indicates a diffusion control

this is analogous to the variation of i_p with $t^{-1/2}$ in chronoamperometry. By analogy, the cath current and peak potential for an oxidation (Red above) are:

$i_{p,a} = (2.69 \cdot 10^5) n^{3/2} A D_R^{1/2} v^{1/2} C_R^*$ $E_{p,a} = E_{1/2} + 1.109 \frac{RT}{nF} = E_{1/2} + \frac{0.0215}{n}$

$\Rightarrow |\Delta E_p| = E_{p,c} - E_{p,a} = \frac{0.056 V}{n}$

Methods for determining the proper baseline for i_p measurements:



Nicholson semiempirical formula

$\frac{i_{p,c}}{i_{p,a}} = \left(\frac{i_{p,c}^c}{i_{p,a}^c}\right) + \frac{0.4463 i_0}{i_{p,a}} + 0.0216$

Linear sweep voltammetry for a slow electrochemical reaction

Case of a reduction: Ox is the only species present in solution

Fully irreversible: with $\eta > 0.12n$, the inverse reaction (oxidation of red) can be neglected

We have established that $C_0(0,t) = C_0^* - \frac{1}{(\pi D_0)^{1/2}} \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau$

$\frac{i}{nFA} = -k_r C_0(0,t) = -k_r^0 C_0(0,t) \exp\left(-\frac{\alpha_r n F E}{RT}\right)$
 $= -k_r C_0(0,t) \exp\left(-\frac{\alpha_r n F E_i}{RT}\right) \exp\left(\frac{k_r n F v t}{RT}\right) = k_r^1 C_0(0,t) \exp \beta t$

non let: $\begin{cases} f(t) = g(\beta t) \\ z = \beta \tau = \frac{\alpha_r n F v}{RT} \tau \end{cases} \Rightarrow \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau \Rightarrow \int_0^{\beta t} \left(t - \frac{z}{\beta}\right)^{-1/2} \frac{g(z)}{\beta} dz = \beta^{-1/2} \int_0^{\beta t} (\beta t - z)^{-1/2} g(z) dz$

$C_0(0,t) = C_0^* - \frac{1}{(\pi D_0)^{1/2}} \int_0^t (t-\tau)^{-1/2} f(\tau) d\tau \Rightarrow C_0(0,t) = C_0^* - \frac{1}{(\beta \pi D_0)^{1/2}} \int_0^{\beta t} (\beta t - z)^{-1/2} g(z) dz$

$$\frac{C_0(0,t)}{C_0^*} = 1 - \frac{1}{C_0^* (\beta \pi D_0)^{1/2}} \int_0^{\beta t} (\beta t - z)^{-1/2} g(z) dz \quad \chi(z) = \frac{g(z)}{C_0^* (\beta \pi D_0)^{1/2}} \quad \frac{C_0(0,t)}{C_0^*} = 1 - \int_0^{\beta t} \frac{\chi(z)}{(\beta t - z)^{1/2}} dz$$

$$\chi(z) = \frac{g(z)}{C_0^* (\beta \pi D_0)^{1/2}} = - \frac{i(\beta t)}{nFA C_0^* (\beta \pi D_0)^{1/2}}$$

$$i(\beta t) = -nFA C_0^* (\beta \pi D_0)^{1/2} \chi(\beta t) = -nFA C_0^* \left(\frac{\alpha r n F v \pi D_0}{RT} \right)^{1/2} \chi(\beta t) = -nFA \pi^{1/2} D_0^{1/2} v^{1/2} C_0^* \left(\frac{\alpha r n F}{RT} \right)^{1/2} \chi(\beta t)$$

⇒ The current is still proportional to C and to v^{1/2}

π^{1/2} χ(βt) goes through a maximum of 0.4953

$$i_{p,c} = - (2.99 \times 10^5) \times n (\alpha r n)^{1/2} A D_0^{1/2} v^{1/2} C_0^* \quad \rightarrow \text{Calculation of } n \text{ from } i_p$$

$$E_{p,c} = \frac{-RT}{\alpha r n F} \left(0.780 - \ln \frac{k^0}{D_0^{1/2}} + \ln \left(\frac{\alpha r n F v}{RT} \right)^{1/2} \right)$$

$$= E^0 - \frac{RT}{\alpha r n F} \left(0.780 - \ln \frac{k^0}{D_0^{1/2}} + \ln \left(\frac{\alpha r n F v}{RT} \right)^{1/2} \right) \quad \text{with } k^0 = k^0 \exp \left(\frac{-\alpha r n F E^0}{RT} \right)$$

⇒ Calculation of k⁰ if n is known.

One can define E_{p,c/2} as the potential where the current is at half the peak value.

(i_{p/2}).

$$\Rightarrow \bar{E}_{p,c} - E_{p/2} = \frac{1.157 RT}{\alpha r n F} = \frac{0.048}{\alpha r n}$$

$$i_{p,c} = -0.227 nFA C_0^* k^0 \exp \left(\frac{-\alpha r n F}{RT} (E_{p,c} - E^0) \right)$$

⇒ Calculation of n from ln i_p = f(E_p - E⁰)
a slope of -αr n F / RT and an intercept proportional to k⁰.

This expression of i_{p,c} is obtained upon combining:

$$i = -nFA \pi^{1/2} D_0^{1/2} v^{1/2} C_0^* \left(\frac{\alpha r n F}{RT} \right)^{1/2} \chi(\beta t) \quad \text{and} \quad E_{p,c} = E^0 - \frac{RT}{\alpha r n F} \left(0.780 - \ln \frac{k^0}{D_0^{1/2}} + \ln \left(\frac{\alpha r n F v}{RT} \right)^{1/2} \right)$$

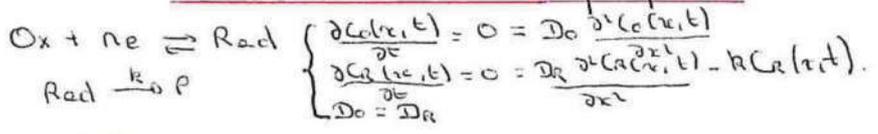
one of an oxidation: Red is the only species present in solution

$$i_{p,a} = (2.99 \times 10^5) n (1 - \alpha r)^{1/2} n^{1/2} A D_R^{1/2} v^{1/2} C_R^*$$

$$i_{p,a} = 0.227 nFA C_R^* k^0 \exp \left(\frac{\alpha r n F}{RT} (E_{p,a} - E^0) \right)$$

Coupled chemical processes

EC; mechanism in stationary regime



Case of a reduction

$$\begin{cases} C_R(x,0) = 0 & \lim_{x \rightarrow \infty} C_R(x,t) = 0 \\ C_O(x,0) = C_0^* & \lim_{x \rightarrow \infty} C_O(x,t) = C_0^* \\ C_P(x,0) = 0 & \lim_{x \rightarrow \infty} C_P(x,t) = 0 \end{cases}$$

Calculation of C_O(x)

$$\frac{\partial^2 C_O(x,t)}{\partial x^2} = 0 \Rightarrow \text{The concentration prof. } C_O(x) \text{ will be linear} \Rightarrow C_O(x) = C_O(0) - \frac{x}{\delta} (C_O(0) - C_0^*)$$

one can use the diffusion layer model where

$$i = -nFA D \left(\frac{\partial C_O(x)}{\partial x} \right)_{x=0} = - \frac{nFA D}{\delta} (C_O(0) - C_0^*)$$

The flux conservation at the electrode gives $-D \left(\frac{\partial C_O(x)}{\partial x} \right)_{x=0} = D \left(\frac{\partial C_R(x)}{\partial x} \right)_{x=0} = \frac{i}{nFA}$

$$\text{Calculation of } C_R(x) \text{ requires to solve } 0 = D \frac{\partial^2 C_R(x,t)}{\partial x^2} - k C_R(x,t) \Rightarrow \frac{\partial^2 C_R(x,t)}{\partial x^2} = \frac{k}{D} C_R(x,t)$$

$$\Rightarrow C_R(x) = X \exp \left(-\sqrt{\frac{k}{D}} x \right) + Y \exp \left(\sqrt{\frac{k}{D}} x \right) \text{ with } X, Y \text{ constants.}$$

$$\text{Flux conservation at the electrode: } D \left(\frac{\partial C_O(x)}{\partial x} \right)_{x=0} = -D \left(\frac{\partial C_R(x)}{\partial x} \right)_{x=0}$$

$$\text{leads to: } (C_0^* - C_O(0)) = X \sqrt{\frac{k}{D}} - Y \sqrt{\frac{k}{D}}$$

$$\text{Also } \lim_{x \rightarrow \infty} C_R(x) = 0 \Rightarrow C_R(\delta) = 0 \Rightarrow C_R(\delta) = X \exp \left(-\sqrt{\frac{k}{D}} \delta \right) + Y \exp \left(\sqrt{\frac{k}{D}} \delta \right) = 0$$

$$\frac{C_0^* - C_O(0)}{\delta} = X \sqrt{\frac{k}{D}} - Y \sqrt{\frac{k}{D}} \quad \text{Further calculation requires to introduce the dimensionless parameter: } \lambda = \frac{k \delta^2}{D}$$

$$\frac{[Co^{2+} - Co(O)]}{\delta} = X \sqrt{\frac{R}{D}} - Y \sqrt{\frac{R}{D}} \quad \lambda = \frac{k\delta^2}{D}$$

$$C_a(\delta) = X \exp(-\sqrt{\frac{R}{D}} \delta) + Y \exp(\sqrt{\frac{R}{D}} \delta) = 0$$

$$\frac{[Co^{2+} - Co(O)]}{\sqrt{\lambda}} = X - Y$$

$$X \exp(-\sqrt{\lambda}) + Y \exp(\sqrt{\lambda}) = 0$$

$$C_a(0) = X + Y = \frac{[Co(O)] - Co^{2+}}{\sqrt{\lambda}} \left(\frac{1 - \exp(\sqrt{\lambda})}{1 + \exp(\sqrt{\lambda})} \right) = \frac{1 - \exp(\sqrt{\lambda})}{1 + \exp(\sqrt{\lambda})} Y$$

$$C_a(0) = X + Y = \frac{[Co^{2+} - Co(O)]}{\sqrt{\lambda}} \frac{\tanh(\sqrt{\lambda})}{1 + \exp(\sqrt{\lambda})}$$

ernst $\rightarrow \exp\left(\frac{nF(E - E^0)}{RT}\right) = \exp(f) = \frac{C_a(0)}{C_a(0)} \rightarrow \exp(f) = \frac{C_a(0)}{[Co^{2+} - Co(O)] \frac{\tanh(\sqrt{\lambda})}{\sqrt{\lambda}}} = \frac{C_a(0) \sqrt{\lambda}}{[Co^{2+} - Co(O)] \tanh(\sqrt{\lambda})}$

$$E = E^0 + \frac{RT}{nF} \ln\left(\frac{C_a(0)}{Co^{2+} - Co(O)}\right) + \frac{RT}{nF} \ln\left(\frac{\sqrt{\lambda}}{\tanh(\sqrt{\lambda})}\right)$$

$$\Rightarrow E = E^0 + \frac{RT}{nF} \ln\left(\frac{\sqrt{\lambda}}{\tanh(\sqrt{\lambda})}\right) + \frac{RT}{nF} \ln\left(\frac{i - i_0}{i}\right) \text{ with } i = nFA D \left(\frac{\partial C_a}{\partial x}\right)_{x=0} = \frac{nFA D}{\delta} (Co^{2+} - Co(O))$$

The equation is similar to that obtained in the absence of chemical step but with E values shifted by: $\Delta E = \frac{RT}{nF} \ln\left(\frac{\sqrt{\lambda}}{\tanh(\sqrt{\lambda})}\right)$

The apparent formal potential is then: $E_{app}^{0'} = E^0 + \frac{RT}{nF} \ln\left(\frac{\sqrt{\lambda}}{\tanh(\sqrt{\lambda})}\right)$
 λ is the dimensionless kinetic parameter which determines the amplitude of the potential shift $\lambda = \frac{k\delta^2}{D}$.

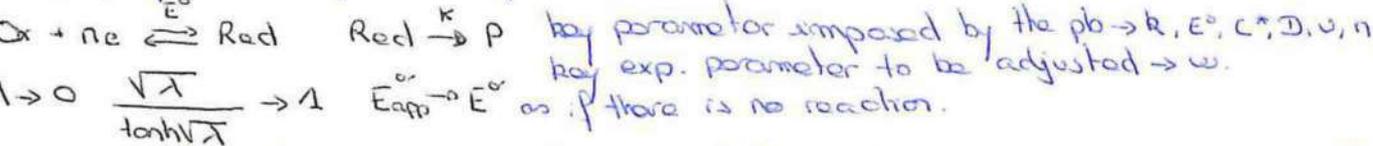
$$\lambda \rightarrow \infty \quad \tanh(\lambda) \rightarrow 1 \quad \Delta E \rightarrow \frac{RT}{2nF} \ln \lambda = 2,3 \frac{RT}{2nF} \log \lambda \quad \text{with } \ln \sqrt{\lambda} = \frac{1}{2} \ln \lambda$$

At 25°C for n=1 $\Delta E \rightarrow 0,03 \log \lambda$

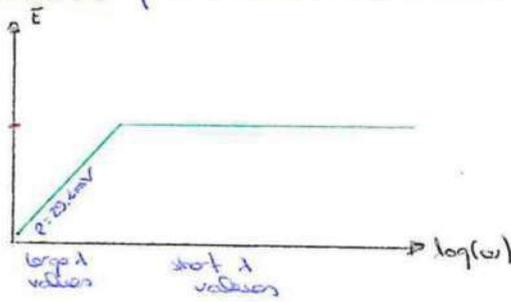
$\lambda = \frac{k\delta^2}{D}$ for RDE $\begin{cases} i_{lim} = 0,0620 nFA D^{1/2} \omega^{1/2} C^* \\ \delta_0 = 1,61 D^{1/3} \omega^{-1/2} \nu^{-1/6} C^* \\ \Rightarrow \lambda \text{ varies with } 1/\omega \end{cases}$

λ varies with δ^2
 $E_{app}^{0'} = f(\log \omega)$ gives a straight line with a slope
 $p = \frac{-2,3 RT}{2F} = -1,15 RT = -29,2 \text{ mV/decade}$

\Rightarrow Diagnostic of an ECi process.



This happens for instance with RDE when the rotation rate gets very large, the diffusion layer is so small that the chemical step has no effects. Mass transport is much faster than the kinetics of the chemical reaction.



Allows to reveal the existence of an ECi mechanism and eventually to estimate the E^0 value if λ is small enough.